Appendix C

Bridge Memorandum



# GRAVINA ISLAND ACCESS

AMENDMENT № 23, ACTIVITY 001, TASK 20 – ENGINEERING ESTIMATES



July 2009

## TABLE OF CONTENTS

BRID	OGE ACTIVITY SUMMARY	1
Tas	sk 20-1 - Review of the EIS Alignments and Structure Types	1
Tas	sk 20-2 - Review of the EIS Quantities	1
Tas	sk 20-3 - Update of the EIS Cost Estimates	2
Tas	sk 20-4 - Consideration of a Steel Structure Alternative at the	
	F3 West Channel Crossing	2
Tas	sk 20-5 - Consideration of an F3 Variant	4
Tas	sk 20-6 - Consideration of a C3-4 Variant	5
Obs	servations	5
Tas Tas	F3 West Channel Crossing sk 20-5 - Consideration of an F3 Variant sk 20-6 - Consideration of a C3-4 Variant	4 5

## PLAN, ELEVATION AND SECTION SKETCHES

Alignment F3 Steel Cable-Stayed Alternative at West Channel	7
Alignment F3 Steel Drop-in Span Alternative at West Channel	8
Alignment F3 with Approach Embankment at West Channel (Segmental)	9
Alignment F3 with Approach Embankment at West Channel (Cable-Stayed)	10
Alignment F3 with Approach Embankment at East Channel (Segmental)	11
Alignment F3 with Approach Embankment at East Channel (Cable-Stayed)	12
Alignment C3-4 with Approach Embankment at Airport (Option A)	13
Alignment C3-4 with Approach Embankment at Airport (Option B)	14

# SUPPORTING QUANTITY AND COST INFORMATION

Adjusted and Updated Costs for EIS Alternates (F1, F3, C3a, C3b, C4, and D1)	. 15
Costs for Variant Alternates (F3 and C3-4)	.16
F3 Steel Cable-Stayed Cost	. 18
F3 Steel Drop-in Span Cost	. 19
F1 Updated Cost	. 20
Cofferdam and Bubbler System Cost	. 21

## LIST OF TABLES

Table 1 - Estimate of Probable Bridge Construction Cost – EIS Alignments	.2
Table 2 -Estimate of Probable Bridge Construction Cost – F3 West	
Channel Alternatives	4
Table 3 -Estimate of Probable Bridge Construction Cost – F3 Variants	4
Table 4 -Estimate of Probable Bridge Construction Cost – C3-4 Variants	.5

#### BRIDGE ACTIVITY SUMMARY

Amendment #23 was issued for the purpose of producing a Supplemental Environmental Impact Statement (SEIS). From a bridge engineering perspective, the SEIS is to evaluate the previously identified alignment alternatives and determine if any adjustments are feasible/appropriate with respect to providing a more economical alternative. The SEIS is also to update the costs for the identified alternatives from 4<sup>th</sup> quarter 2004 to 1<sup>st</sup> quarter 2008. The specific bridge activities are as follows.

#### Task 20-1 - Review of the FEIS Alignments and Structure Types

This task consisted of the review of the Final Environmental Impact Statement (FEIS) alignments (F1, F3, C3a, C3b, C4, and D1) to determine if there were any minor adjustments that could be made to the alignment and span arrangements to improve the economy of the alternatives. It was determined that while minor adjustments could be incorporated, none of the adjustments substantially revised the bridge configurations proposed in the FEIS. As a result it was concluded that adjustments to the alternatives in the FEIS were not warranted as they would not afford any meaningful cost reductions for the proposed facilities.

#### Task 20-2 - Review of the FEIS Quantities

This task involved the review of the quantity determinations for the cost estimates in the FEIS. Specifically, the bridge quantities for preferred Alignment F1 were checked for reasonableness based on the proposed structures and available data for similar/comparable structures that have been constructed in the past. The quantities for reinforcing steel and post-tensioning were reduced somewhat as a result of this review. The quantity verification effort for F1 was then pro-rated to the other FEIS alignments (F3, C3a, C3b, C4, and D1) with adjustments as required to accommodate the variations between the respective alternatives and F1 (as was done for the FEIS effort).

The quantities for the single bridge alignments (C3a, C3b, C4 and D1) were also adjusted to address the curvature of the approach spans (and in some cases where the curvature carries onto the main span over the navigational channel). While the curvature was previously recognized, there were no attempts to quantify the cost implications because it was indicated that level of refinement was unwarranted based on the assumption that funding was available for the preferred F1 alignment. Without additional computational effort to advance the level of design (from a conceptual level to a level in excess of a preliminary design effort) it is difficult to quantify the cost implications attributable to the curvature. Let it suffice to say that the conditions are essentially unprecedented in balanced cantilever construction and would result in severe torsional considerations. It is anticipated that the superstructure in the curved sections would have to be strengthened considerably to provide the required capacity for the cantilever condition. For estimating purposes it was assumed that the structural quantities (concrete, reinforcing steel, and post-tensioning) in the curved sections would increase by 50 percent. It was also assumed that the quantities for the main piers (foundations, concrete, reinforcing steel, and post-tensioning) would increase by 100 percent and an additional pier would be

required at the back-span. As a result, there is a significant increase in the cost of the single bridge alignments above and beyond the cost escalation considerations from 2004 to 2008.

#### Task 20-3 - Update of the FEIS Cost Estimates

This task involved adjusting the cost estimates developed for the FEIS alternatives from the 4<sup>th</sup> quarter of 2004 to the 1<sup>st</sup> quarter of 2008. The effort was based on the previously determined quantities adjusted as noted above, and consideration of contractor operations. These additional considerations included the cost of cofferdams and bubbler systems to allow year-round in-water construction, and additional sets of form travelers to facilitate more efficient construction. The cost of fenders at in-water piers was also included.

In summary, there is approximately a 20% and 22% increase in structure cost for the F1 and F3 alignments respectively over the estimates provided in the FEIS, 17% of which is essentially attributable to the cost of inflation (i.e., the quantity adjustments had a relatively minimal impact). The balance of the increase in cost is attributable to provisions for cofferdams, bubbler systems, additional form travelers, and fenders. An increase of 55% to 70% is presented for C3a, C3b, C4 and D1. That increase is similarly due to the cost of inflation, cofferdams, bubbler systems, additional form travelers, and fenders, but was also significantly impacted by the adjustment in quantities to account for the effects of the curvature of the alignments.

Alignment	Substructure Cost	Superstructure Cost	Total Cost	Cost/SF Deck Area		
F1 West	\$54M	\$47M	\$101M	\$796		
F1 East	\$75M	\$64M	\$139M	\$796		
F3 West	\$55M	\$47M	\$102M	\$805		
F3 East	\$44M	\$38M	\$82M	\$805		
C3a	\$175M	\$160M	\$335M	\$961		
C3b	\$139M	\$100M	\$240M	\$1101		
C4	\$170M	\$141M	\$311M	\$1216		
D1	\$110M	\$85M	\$195M	\$1060		

#### Table 1 -Estimate of Probable Bridge Construction Cost – FEIS Alignments\*

\* See Supporting Quantity and Cost Information (some rounding will occur).

# Task 20-4 - Consideration of a Steel Structure Alternative at the F3 West Channel Crossing

Steel bridge alternatives were evaluated for the purpose of establishing a cost per square foot basis of comparison to the proposed concrete segmental bridge in the FEIS. The consideration of various steel alternatives was as noted below. A brief summary discussion is provided relative to each of the alternatives. Note that the "per square foot cost" for the alternatives was based on recent similar projects and historical data for similar type bridges. The derived cost is based on those comparable costs adjusted for geographic location, date of construction, and project dissimilarities that would impact cost.

The previous cost estimating exercises associated with this project indicated that the cost of in-water substructure, and in particular deep-water construction in close proximity to the track lines, resulted in the greatest contribution to the overall cost of the bridge (due to deep-water construction considerations and ship impact design considerations). Given that assessment, it was deduced that the avenue to a more economical facility was to minimize deep-water foundations and cruise ship impact considerations, or eliminate in-water construction altogether. Note that in-water construction is also constrained by environmental considerations (work in marine waters may occur July 1<sup>st</sup> through February 28<sup>th</sup>.except for blasting, dredging, and pile driving which can occur only between November 1<sup>st</sup> and February 28<sup>th</sup>) and would lengthen the number of construction seasons required to complete any alternative requiring in-water construction unless cofferdams and bubbler systems (or other similar mitigation measures) could be successfully implemented.

The following traditional steel bridge alternatives were considered: girder, arch, truss, and cable-stayed. The first three alternatives (girder, arch, and truss type bridges) were dropped from consideration by inspection (based on the physical requirements of the site, physical limitations of the systems, and experience). Specifically, a girder bridge is not an appropriate bridge type given the required span; an arch bridge is not an appropriate bridge type given the physical characteristics of the site and the required span and navigational opening; and, a truss bridge is not an appropriate bridge type given the required span, and initial and life-cycle cost considerations.

While not an ideal site from a topographical perspective, a cable-stayed alternative is an appropriate bridge type for this location. A number of variations were considered before the proposed configuration was deemed the most beneficial. The variations included a shorter main span of 1100 feet that required an in-water pier near Gravina Island along with several approach spans, and a 1600-foot main span alternative (page 7) that resulted in both piers on land with no need for approach piers. It was concluded that the latter configuration is the most beneficial as it simplifies the structure, eliminates in-water construction, and eliminates ship impact considerations on the design of the bridge. Traditionally, longer spans translate into more cost, but we are of the opinion that the above considerations offset the cost effect of the longer span. Also note that a span of 1100 to 1600 feet is well within the economical range of a cable-stayed bridge. (See Plan, Elevation, and Section Sketches.)

As a variation of the concrete segmental box girder bridge proposed in the FEIS, a similar concrete segmental box girder bridge utilizing a steel drop-in span over the navigational channel was also considered. The concrete segmental box girder alternative with a steel drop-in span takes advantage of the economy of concrete segmental construction and the lighter weight of a structural steel section. The reduction in dead load due to the steel drop-in span (page 8) increases span capability over that of a traditional concrete segmental box girder. While the proposed configuration still requires in-water construction, it eliminates the need for a deep-water pier adjacent the navigational opening. Elimination of deep-water construction and the need to design for cruise ship impact offsets the higher unit cost of the steel drop-in section. (See Plan, Elevation, and Section Sketches.)

Alternative	Substructure Cost	Superstructure Cost	Total Cost	Cost/SF Deck Area
Stayed	\$32M	\$112M	\$144M	\$850
Drop-in	\$48M	\$58M	\$106M	\$793

#### Table 2 -Estimate of Probable Bridge Construction Cost – F3 West Channel Alternatives\*

\* See Supporting Quantity and Cost Information.

#### Task 20-5 - Consideration of an F3 Variant

This task involved re-assessment of the F3 alignment bridge alternatives assuming that previously imposed constraints could be adjusted. These constraints included the use of approach embankment to water's edge, approach embankment beyond water's edge, and relocation of track lines. The implementation of approach embankment is to take advantage of readily available and easily assessable rock material in the area. The use of embankment allows the length of structure to be reduced considerably taking advantage of the lower unit cost of the embankment. For the configuration where the embankment construction extends beyond water's edge, it was assumed that it was practical and economically feasible to place embankment to a depth of 40 feet. The engineering parameters that were assumed were that embankment material above water's edge could be placed and maintained at a 2:1 slope. Material placed below water was assumed to be placed at 3:1, and on the slope of the bottom at the toe of the embankment at no greater than 10%. It was assumed that the fills that extended beyond water's edge would be constructed from landside out using the advancing embankment as egress, except where the bottom exceeds 10% where it was assumed that the embankment would have to be built from the water on barges and constructed back towards land to buttress the construction. The limits of the embankment were not permitted to encroach into the navigation opening above -40 feet below MLLW.

Such consideration at F3 resulted in two revised bridge configurations. One lends itself to a cable-stayed alternative with a single deep water pylon and symmetric spans of 880 feet (page 10) over West Channel. The other lends itself to a segmental concrete box girder with a main span of 700 feet (page 9). Costs were also developed for a cable-stayed and a segmental concrete box girder structures over East Channel (pages 12 and 11). A plan, elevation and typical section of each configuration are provided herein and the associated construction cost estimates are provided below.

#### Table 3 -Estimate of Probable Bridge Construction Cost – F3 Variants\*

Alternative	Substructure Cost	Superstructure Cost	Total Cost	Cost/SF Deck Area
West Segmental	\$52M	\$32M	\$84M	\$958
East Segmental	\$78M	\$32M	\$110M	\$1,261
West Stayed	\$42M	\$59M	\$101M	\$1,113
East Stayed	\$43M	\$57M	\$100M	\$1,149

\* See Supporting Quantity and Cost Information (some rounding will occur).

#### Task 20-6 - Consideration of a C3-4 Variant

A refinement of alignment C3a using the Borough's proposed Bypass (or Bench) Road to Signal Road near the Wal-Mart parking lot rather than a large cut to North Tongass Avenue will save the cost of providing a curved structure at the east abutment. In addition, if the track line location is allowed to be adjusted, the main span and back spans of the crossing can be constructed on tangent. The curve at the transition pier and west approach tangent could then be constructed using precast concrete girders. Several variations are possible at the west approach. Chorded precast girders (page 14) or castin-place concrete girders built on falsework (page 13) can be used on the curved portion of the alignment. The tangent spans can be comprised of conventional precast girder spans to approximately 150 feet or spliced precast girders can be used to reduce the number of piers. (See Plan, Elevation, and Section Sketches.)

# Table 4 -Estimate of Probable Bridge Construction Cost – C3-4 Variants\*

Alternative	Substructure Cost	Superstructure Cost	Total Cost	Cost/SF Deck Area
A: CIP & PC	\$104M	\$60M	\$164M	\$765
B: PC	\$112M	\$53M	\$165M	\$770
* Cas Commenting Or	antita and Cast Infam			

\* See Supporting Quantity and Cost Information.

#### **Observations**

The cost of providing an all-weather hard link from Revilla Island to Gravina Island on any of the previously established FEIS alignments is more costly today than it was in 2004. This is primarily attributable to inflation, although it can be noted that the costs of the structures on the single bridge alignments have also increased substantially due to the attempt to quantify the effects of the curvature of the approaches.

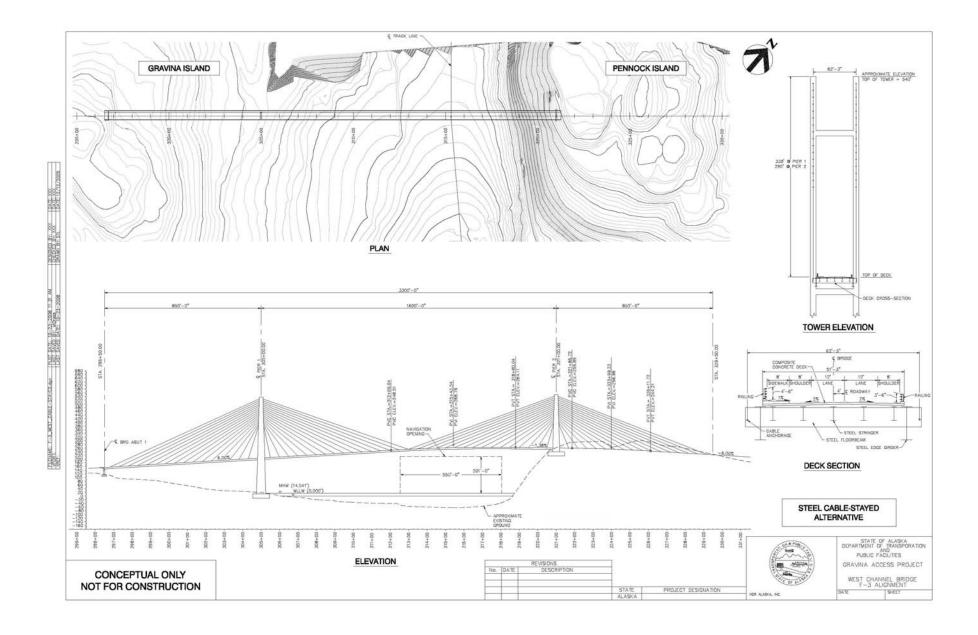
It should also be noted that based on the evaluation of a steel cable-stayed and steel drop-in span alternative for the crossing of the west channel of the F3 alignment, consideration of previously dismissed structure types may provide a more economical solution than the currently proposed concrete segmental box girder structure. It is intuitive that a facility that minimizes/eliminates in-water construction would be a preferred alternative, as long as the configuration did not push the envelope of applicability of the proposed structure type. The reduction/elimination of in-water construction minimizes construction risk, reduces design demands by eliminating cruise ship impact considerations, reduces environmental impacts, and reduces potential construction season restrictions and mitigations measures. The cost estimates provided herein indicate that the steel alternatives are reasonably close in cost to the segmental box girder alternative. Thus, should it be determined that the F3 alignment has merit from a funding perspective, it is recommended that the steel alternatives and segmental concrete box girder alternative be revisited and developed to a level comparable to the segmental concrete box girder alternative on the F1 alignment to insure that structure type selection is based on comparable levels of design development. Note however, even if refinement efforts fail to result in a substantially lower cost estimate for the steel alternatives, the construction risk associated with the steel alternatives would be significantly less than that of the segmental concrete box girder alternative. Less risk generally translates into a lower bid-day price and a lower project close-out cost due to a reduced potential for claims.

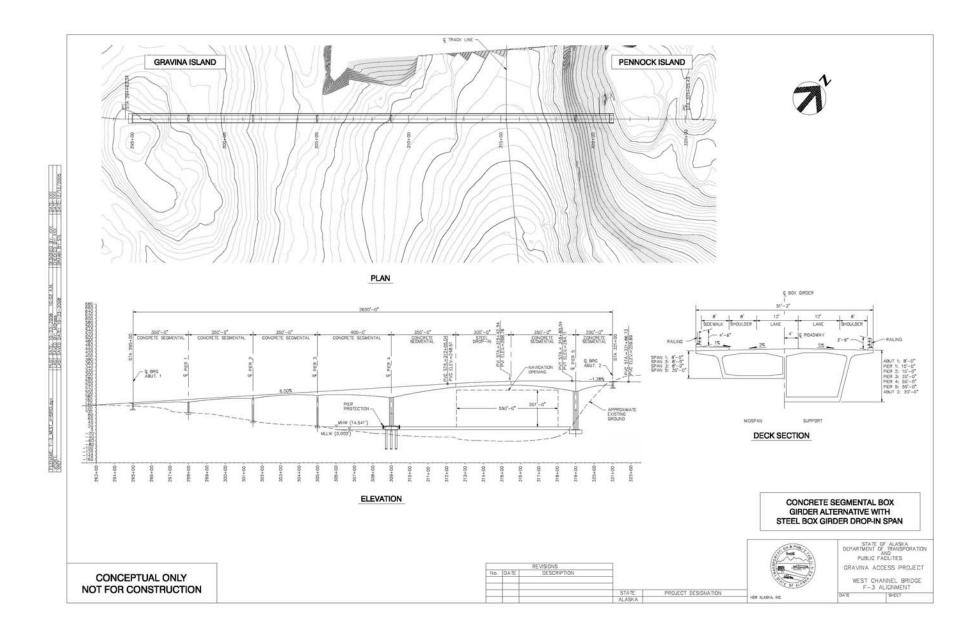
The F3 variant configurations resulted in shorter bridge lengths but higher bridge costs due to additional in-water pier construction required by the revised spans.

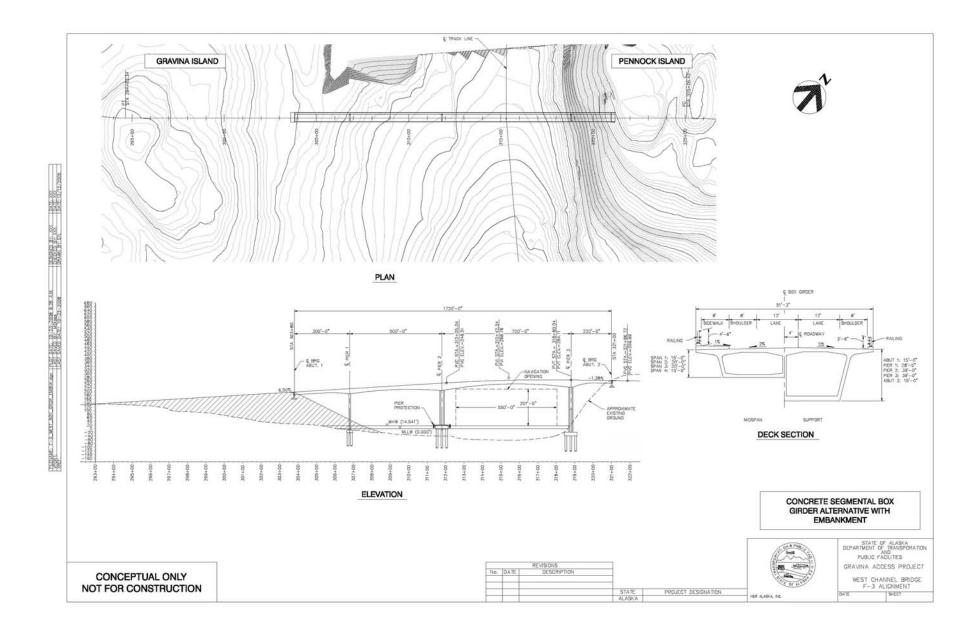
Another observation resulting from this exercise is that a single bridge alternative (on an "airport alignment") is economically competitive if certain allowances are made with respect to some of the previously established design criteria (e.g., design speed, track line location, etc.). Such adjustments allow the cost associated with curvature on the back and/or main spans to be eliminated. In addition to resulting in a lower bridge cost, an airport alignment could conceivably be constructed at a lower overall project cost due to a reduction in cost for roadway and other considerations. However, as noted above for the previous tasks addressed herein, it is important to recognize that while the estimated construction costs for all of the alternatives are reasonably comparative, the basis for the costs vary (i.e., some are based on conceptual level engineering and some are based on proration). Given that, it is recommended that any alternatives that are to be advanced for further study (i.e., formal type study) be developed to a comparable level of design to insure that alternative selection is based on a comparable level of cost estimates.

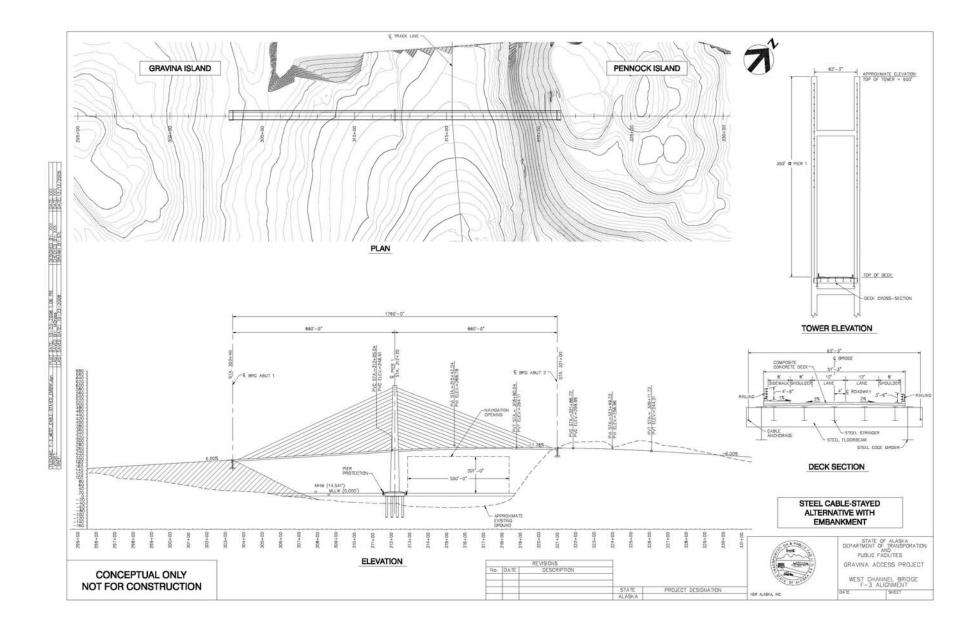
Z:\07072 DOT&PF\19752 Design Build - Gravina\019 - Design\DSR\DDSR for SEIS\Bridge Memo Final 7-31-09.doc

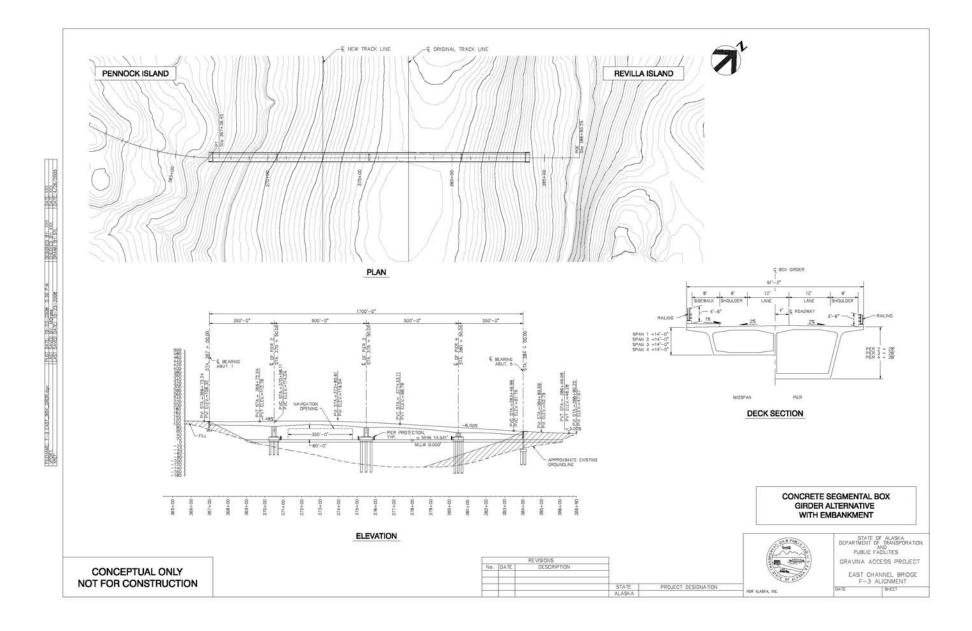
PLAN, ELEVATION AND SECTION SKETCHES

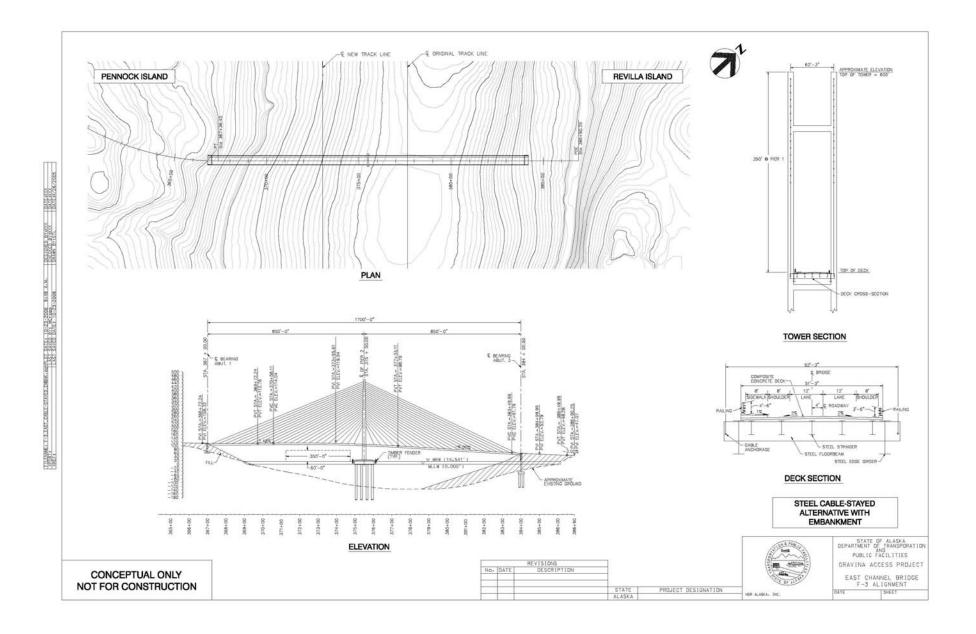


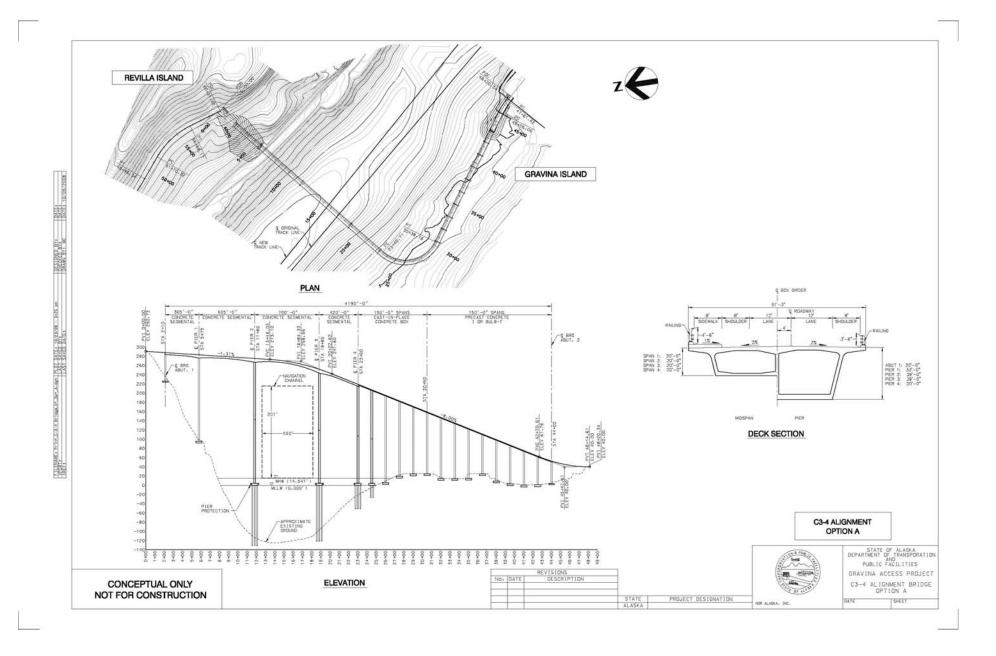


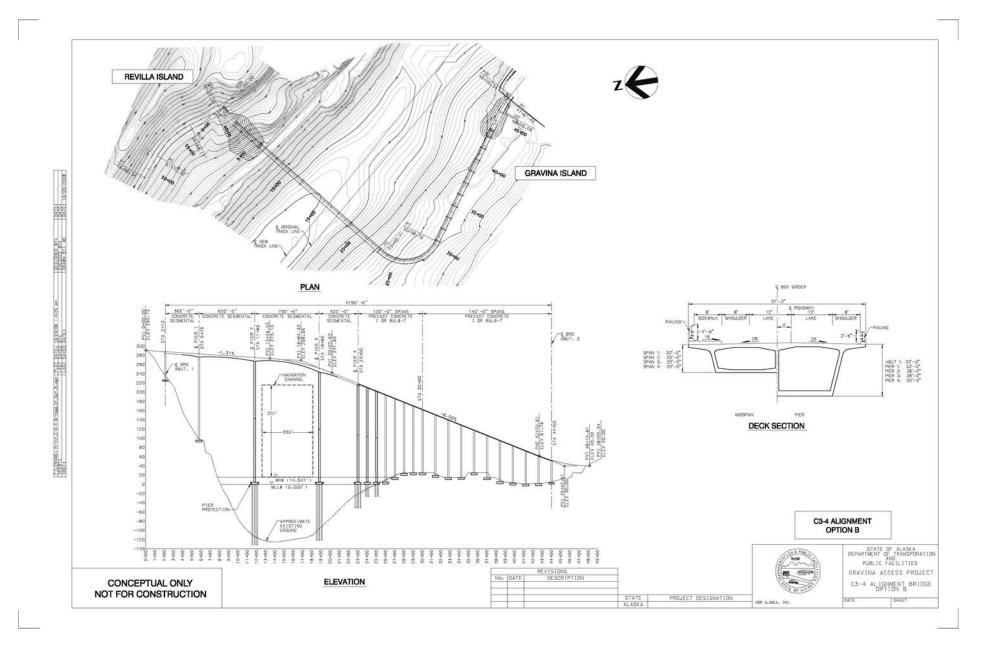












# SUPPORTING QUANTITY AND COST INFORMATION

#### GRAVINA COSTS ADJUSTED BASE ALTERNATES COST ESCALATED TO 1st

QTR. 2008																									
	SHIP IMPACT	UofM		QUANTITY	C-3A UNIT	AMOUNT		OUANTITY	C-3B UNIT	AMOUNT		OUNTITY	C-4 UNIT	AMOUNT	-	CALATED 8		QUANT		CALATED		011			
	INIPACI			QUANTITY				QUANTITY				QUANTITY			QUANTITY			QUANTI			MOUNT				AMOUNT
BASE SUB-STRUCTURE		SF		348,500.00 \$	413.61 \$	144,143,085		217,813.00 \$	413.61 \$	90,089,635		256,250.00 \$	413.61 \$	105,987,563		\$ 413.61	\$ 52,251,765 \$ 72,071,543		<u>00</u> \$4	413.61 \$ 413.61 \$		184	l,500.00 \$	430.23	\$ 79,377,435
BASE SUPERSTRUCTURE		SF		348,500.00 \$	364.18 \$	126,916,730		217,813.00 \$	364.18 \$	79,323,138		256,250.00 \$	364.18 \$	93,321,125	W 126,331.00 E 174,250.00 300,581.00	\$ 364.18	\$ 46,007,224 \$ 63,458,365		<u>31</u> \$3	364.18 \$ 364.18 \$		184	l,500.00 \$	364.18	\$ 67,191,210
ADD FOR CURVED DECK		SF	premium	174,250.00 \$	182.09 \$	31,729,183	premium	108,906.50 \$	182.09 \$	19,830,785	premium	256,250.00 \$	182.09 \$	46,660,563	000,001100			220,0				premium 92	2,250.00 \$	182.09	\$ 16,797,803
ADD PIER 120 FOOT WATER	YES	EACH		- \$	24,178,372.00 \$	-		\$ 2	24,178,372.00 \$	-	premium	1.00 \$	24,178,372.00 \$	24,178,372											
ADD PIER 80 FOOT WATER	YES	EACH		\$	21,558,053.00 \$	-	premium	1.00 \$ 2	21,558,053.00 \$	21,558,053		\$	21,558,053.00 \$	-											
ADD PIER 50 FOOT WATER	YES	EACH	premium	n 1.00 \$	18,894,543.00 \$	18,894,543	new	1.00 \$ 1	8,894,543.00 \$	18,894,543	premium	n 1.00 \$	18,894,543.00 \$	18,894,543								new	1.00 \$ 18	,894,543.00	\$ 18,894,543
ADD PIER 20 FOOT WATER	NO	EACH	new	1.00 \$	6,223,205.00 \$	6,223,205		\$	6,223,205.00 \$	-	new	2.00 \$	6,223,205.00 \$	12,446,410								new	1.00 \$ 6	,223,205.00	\$ 6,223,205
BASE TOTAL		SF																							
BASE EAST CHANNEL		SF													174,250.00										
BASE WEST CHANNEL		SF													126,331.00										
COFFERDAM AND BUBBLER					\$	5,474,122	4 piers		\$	8,415,232	4 piers		\$	8,415,232		2 piers	\$ 4,207,616	2 piers		\$	4,207,616	3 pi	ers		\$ 5,474,122
FENDER EXTRA FORM TRAVELERS					\$	470,760 1,176,900	_		\$ \$	470,760 1,176,900			\$ \$	470,760 1,176,900			INC \$ 1,176,900			\$ \$	823,830 1,176,900			-	\$ 470,760 \$ 1,176,900
		SF		348,500.00 \$	961.34 \$	335,028,528		217,813.00 \$	1,100.76 \$	239,759,046		256,250.00 \$	1,215.81 \$	311,551,467	300,581.00	\$ 795.70	\$ 239,173,412	228,370	00 \$ 8	804.98 \$ <sup>-</sup>	183,832,248	184	l,500.00 \$	1,060.20	\$ 195,605,978
SUBSTRUCTURE				\$	502.74 \$	175,205,715		\$	640.13 \$	139,428,223		\$	664.95 \$	170,392,880	W 126,331.00 E 174,250.00					435.64 \$ 435.64 \$			\$	598.59	\$ 110,440,065
SUPERSTRUCTURE				\$	458.60 \$	159,822,813		\$	460.63 \$	100,330,823		\$	550.86 \$	141,158,588			\$ 46,501,862 \$ 64,140,626			369.33 \$ 369.33 \$			\$	461.60	\$ 85,165,913
TOTALS					\$	335,028,528			\$	239,759,046			\$	311,551,467	W 126,331.00 E 174,250.00					804.98 \$			\$	1,060.20	\$ 195,605,978

COMMENTS

C3A Adjusted quantities and unit costs to that of revised F-1 and added pier and deck costs for curvature at ends

C3B Did not have original pricing, so developed based on quantities and F-1 pricing with adds for curvature at ends

C4 Adjusted quantities and unit costs to that of revised F-1 and added pier and deck costs for curvature at ends

F1 Escalated quantified unit pricing and adjusted reinforcing and PT quantities

D1 Adjusted quantities and unit costs to that of revised F-1 and added pier and deck costs for curvature at ends

ALL All costs include 20% contingency

GRAVINA CC VARIANT ALTEF COST ESCALATEI	C3 - 4 ALIGNMENT OPTION A				C3 - 4 ALIGNMENT OPTION B				EST CHANNI E SEGMENTAL EMBANKMEN	BOX	F-3 W Steel				
	UofM	QUANTITY	UNIT	AMOUNT	1	QUANTITY	UNIT	AMOUNT	QUANTITY	UNIT	AMOUNT	QUANTITY	UNIT	AMOUNT	
BRIDGE LENGTH	LF	4,190.00				4,190.00			1,720.00			3,300.00			
BASE SUB-STRUCTURE	SF	214,738.00 \$	435.62 \$	93,544,168		214,738.00 \$	468.51 \$	100,606,900	88,150.00 \$	540.95	\$ 47,684,743	169,125.00 -		\$ 30,777,368 \$ -	
BASE SUPERSTRUCTURE	SF	214,738.00	\$	-		214,738.00	\$	-	88,150.00 \$	364.18	32,102,467	169,125.00	\$ 660.33	\$ 111,678,311	
		SEG         107,113.00         \$           CIP         38,437.00         \$           BT         69,188.00         \$	322.00 \$	39,008,412 12,376,714 8,994,440	SEG CIP BT	107,113.00 \$ 107,625.00 \$	364.18 \$ \$ 130.00 \$	-							
COFFERDAM AND BUBBLER	DEEP WATER \$ 2,941,110 SHALLOW WATER \$ 1,266,506	2.00 F 2.00 F		5,882,220 2,533,012		2.00 PIER 3.00 PIER		5,882,220 3,799,518	1.00 PIE 1.00 PIE		_,• , •	- 1.00		\$- \$1,266,506	ò
FENDER	\$ 470,760	4.00 F		1,883,040		4.50 PIER		2,118,420	1.00 PIE		470,760		PIER	\$ - \$ -	=
	SF	214,738.00 \$	764.76 \$	164,222,006		214,738.00 \$	770.27 \$	165,406,721	88,150.00 \$	958.20	\$ 84,465,586	169,125.00	\$ 849.80	\$ 143,722,185	
SUBSTRUCTURE		214,738.00 \$	483.58 \$	103,842,440		214,738.00 \$	523.46 \$	112,407,058	88,150.00 \$	594.02	52,363,119	169,125.00	\$ 189.47	\$ 32,043,874 \$ -	
SUPERSTRUCTURE		214,738.00 \$	281.18 \$	60,379,566		214,738.00 \$	246.81 \$	52,999,662	88,150.00 \$	364.18	32,102,467	169,125.00	\$ 660.33	\$ 111,678,311	
TOTALS		214,738.00 \$	764.76 \$	164,222,006		214,738.00 \$	770.27 \$	165,406,721	88,150.00 \$	958.20	84,465,586	169,125.00	\$ 849.80	\$ 143,722,185	,

All costs include 20% Contingency

#### GRAVINA COSTS VARIANT ALTERNATES COST ESCALATED TO 2008

		STEEL CA	T CHANNEL ABLE -STAYED IBANKMENT		F-3 WEST CHANN CONCRETE SEGMENTAI WITH STEEL DROP-IN-S	F-3 EAST CHANNE CONCRETE SEGMENTAL WITH EMBANKMEN	вох	F-3 EAST CHANNEL STEEL CABLE -STAYED WITH EMBANKMENT			
	UofM	QUANTITY	UNIT	AMOUNT	QUANTITY UNIT	AMOUNT	QUANTITY UNIT	AMOUNT	QUANTITY UNIT	AMOUNT	
BRIDGE LENGTH	LF	1,760.00			2,600.00		1,700.00		1,700.00		
BASE SUB-STRUCTURE	SF	90,200.00 \$	423.79 \$ \$	38,225,858 -	133,250.00 \$ 323.5	59 \$ 43,118,368	87,125.00 \$ 789.68 \$	68,800,870	87,125.00 \$ 438.76 \$	38,226,965	
BASE SUPERSTRUCTURE	SF	90,200.00 \$	651.50 \$	58,765,300	133,250.00 \$ 433.5	6 \$ 57,771,870	87,125.00 \$ 364.18 \$	31,729,183	87,125.00 \$ 656.18 \$	57,169,683	
COFFERDAM AND BUBBLER FENDER	DEEP WATER \$ 2,941,110 SHALLOW WATER \$ 1,266,506 \$ 470,760	1.00 PIE - PIE 1.00 PIE	ER \$	2,941,110 - 470,760	1.00 PIER 1.00 PIER 1.00 PIER	\$ 2,941,110 \$ 1,266,506 \$ 470,760	2.00 PIER \$	2,533,012	1.00 PIER \$ 1.00 PIER \$ 1.00 PIER \$	1,266,506	
	SF	90,200.00 \$	1,113.12 \$	100,403,028	133,250.00 \$ 792.2	26 \$ 105,568,614		109,886,805		5 100,075,024	
SUBSTRUCTURE		90,200 \$	461.62 \$ \$	41,637,728 -	133,250.00 \$ 358.7	70 \$ 47,796,744 \$ -	87,125.00 \$ 897.07 \$		87,125.00 \$ 492.46 \$ \$		
SUPERSTRUCTURE		90,200 \$	651.50 \$	58,765,300	133,250.00 \$ 433.5	6 \$ 57,771,870	87,125.00 \$ 364.18 \$	31,729,183	87,125.00 \$ 656.18 \$	57,169,683	
TOTALS		90,200.00 \$	1,113.12 \$	100,403,028	133,250.00 \$ 792.2	26 \$ 105,568,614	87,125.00 \$ 1,261.25	109,886,805	87,125.00 \$ 1,148.64 \$	5 100,075,024	

All costs include 20% Contingency

GRAVINA PROBABLE COST Cable-Stay F-3 WEST CHANNEL							
Total Length Main Span Length Width Pylon Piers on Land	3,300.0 1,600.0 51.25		169,125	5 SF			
		QTY	UOM		UNIT COST		AMOUNT
Pylon Pier Below Deck Deduct Pier 2 Short Land 12 DS Each		2.00	EA	\$	9,530,000.00	\$ \$	19,060,000.00 (1,050,000.00)
Pylon Above Deck **Concrete	Pier 1	4 707 00	0)/	¢	000.00	۴	4 074 000 00
**Reinforcing (300LB/CY)		1,737.00 521,100.00	CY LB	\$ \$	963.89 1.96	\$ \$	1,674,269.98 1,021,356.00
Pylon Above Deck **Concrete	Pier 2	1,737.00	CY	\$	963.89	\$	1,674,269.98
**Reinforcing (300LB/CY)		521,100.00	LB	\$	1.96	\$	1,021,356.00
End Piers/Abutment		2.00	0)/	¢	C00.40	۴	4 044 740 40
**Concrete **Reinforcing (300LB/CY)		1,760.00 528,000.00	CY LB	\$ \$	688.49 1.96	\$ \$	1,211,742.40 1,034,880.00
Superstructure (Deck less Stays)		169,125.00	SF	\$	432.61	\$	73,165,166.25
**Cable-Stay System		2.00	LS	\$	9,950,000.00	\$	19,900,000.00
Contingency	Sub Super	20% 20%		\$ \$	25,647,874.36 93,065,166.25	\$ \$	5,129,574.87 18,613,033.25
	Ouper	2070		Ψ	33,003,100.23		
TOTAL COST BRIDGE				(does	s not include costs for	\$ coffe	<b>142,455,648.74</b> erdams and bubblers)
Total Unit Cost		169,125.00	SF	(000		\$	842.31
Superstructure		169,125.00		\$	111,678,199.50	\$	660.33
Substructure		169,125.00		\$	30,777,449.24	\$	181.98

pylon factor 1.40

CIP BOX AND DROP-IN-S WEST CHANNE									
Total Length CIP Concrete Box Length Width	2,600.0 300.0 2,300.0 51.25	Feet							
Pylon Piers on Land		071/							
		QTY	UOM		UNIT COST		AMOUNT		
Superstructure CIP Box (from F-1)		117,875.00	SF	\$	364.18	\$ 4	42,927,717.50		
Drop-in-Box (15,375 SF @ 150lb/sf)		2,306,250.00	LB	\$	5.00	\$	11,531,250.00		
Deck Concrete on Steel (12") **Reinforcement Superstructure Total		570.00 228,000.00	CY LB	\$ \$	688.49 <sup>1.96</sup> =	\$ \$	392,439.30 446,880.00	\$	55,298,286.80
Abutments ( 2 each )	Concrete Reinforcement	1,000.00 300,000.00	CY LB	\$ \$	688.49 1.96 <u>-</u>		688,490.00 588,000.00		
Pier 1	Concrete Reinforcement	1,143.00 342,900.00	CY LB	\$ \$	688.49 1.96		786,944.07 672,084.00	\$	1,276,490.00
		,		·				\$	1,459,028.07
Pier 2	Concrete Reinforcement	2,683.00 858,822.00	CY LB	\$ \$	688.49 1.96 _	\$ \$	1,847,218.67 1,683,291.12	\$	3,530,509.79
Pier 3	Concrete Reinforcement	2,683.00 858,822.00	CY LB	\$ \$	688.49 1.96 _	\$ \$	1,847,218.67 1,683,291.12	\$	3,530,509.79
Pier 4 Drilled Shaft 16 Each	Concrete Reinforcement DS Rock Exc DS Concrete DS Reinforcement DS Casing DS Instrumentation Pier Protection	10,127.00 3,037,983.00 1,396.00 3,721.00 1,488,593.00 1,024,896.00 16.00 1.00	CY LB CY LB LB EA EA	\$ \$ \$ \$ \$ \$ \$	688.49 1.96 2,059.58 582.57 1.52 0.98 2,500.00 235,380.00	\$ \$ \$ \$ \$ \$	6,972,338.23 5,954,446.68 2,875,173.68 2,167,742.97 2,262,661.36 1,004,398.08 40,000.00 235,380.00	\$	21,512,141.00
Pier 5	Concrete Reinforcement	3,622.00 1,086,556.00	CY LB	\$ \$		\$ \$	2,493,710.78 2,129,649.76	\$	4,623,360.54
Contingency on Super less F1 Unit Contingency on Substructure		20% 20%			12,370,569.30 35,932,039.19 _			\$	9,660,521.70
TOTAL COST BRIDGE						alc		\$	100,890,848
Total Unit Cost		133,250.00	SF		(aces not inclu	iae c	osts for cofferdar	ns, bu \$	bblers, and fenders) <b>757.15</b>
Superstructure		133,250.00	SF			\$	57,772,401	\$	433.56
Substructure		133,250.00	SF			\$	43,118,447	\$	323.59

#### GRAVINA BRIDGE UPDATED COST ESTIMATE, ALIGNMENT F1 MARCH 3, 2008

ITEM NO.	ΡΑΥ ΙΤΕΜ		EAST QUANTITY	WEST QUANTITY	TOTAL QUANTITY				ESCALATED			
202(2)	Rock Excavation for Structures	auh	E 201	2 540	7 000	0)/	<b>*</b> 50	Ļ	1.1769	•	400 400 00	
203(2)		sub	5,301	2,519	7,820	CY CY	\$50	\$	58.85		460,196.23	
205(1)	Excavation for Structures (above water)	sub	2,150	400	2,550		\$20	\$	23.54		60,021.90	
501(1)	Class A Concrete (Footing)	sub	19,889	8,673	28,562	CY	\$585	\$		\$	19,664,474.91	
501(1)	Class A Concrete (pier) Class A-A Concrete (sidewalk and approach	sub	11,918	5,467	17,385	CY	\$585	\$	688.49	•	11,969,558.38	
501(2)	slab)	sup	1,266	944	2,210	CY	\$675	\$	794.41		1,755,655.29	
501(2)	Class A-A Concrete (Segmental box)	sup	26,593	15,441	42,034	CY	\$855	\$	1,006.25		42,296,457.54	
501(20)	Class DS Concrete (drilled shaft concrete)	sub	14,195	3,694	17,889	CY	\$495	\$	582.57	\$	10,421,714.97	
501(21)	DS Grout (drilled shaft grout)	sub	0	0	0		\$700	\$	823.83		•	
502(1)	Post-Tensioning (box girder bridge)	sup	4,520,770	2,624,970	7,145,740	LB	\$2.75	\$	3.00	\$	21,437,220.00	REVISED PRICING
502(1)	High Strength Bars	sup	151,845	88,167	240,012	LB	\$4.00	\$	13.08	\$	3,139,356.96	REVISED PRICING
503(1)	Reinforcing Steel - Superstr	sup	5,318,554	3,088,200	8,406,754	LB	\$1.43	\$		\$	12,778,266.08	REVISED PRICING
503(1)	Reinforcing Steel - Substr	sub	6,572,445	1,710,452	8,282,897	LB	\$1.43	\$		\$	12,590,002.74	REVISED PRICING
503(2)	Epoxy Coated Reinforcing Steel - Superstr	sup	1,329,638	772,050	2,101,688	LB	\$1.66	\$	1.96	\$	4,112,154.86	
503(2)	Epoxy Coated Reinforcing Steel - Substr	sub	10,733,995	4,788,700	15,522,695	LB	\$1.66	\$	1.96	\$	30,371,646.83	
	Bearings	sup	10	4	14	EACH	\$25,000	\$	40,000.00	\$	560,000.00	REVISED PRICING
	Modular Joints	sup	154	102.50	256	LF	\$1,500	\$	1,765.35	\$	452,370.94	
507(2)	Pedestrian Railing (3 Tube incl curb)	sup	6,800	4,930	11,730	LF	\$150	\$	176.54	\$	2,070,755.55	
508(1)	Waterproofing Membrane	sup	174,250	126,331	300,581	SF	\$1.25	\$	1.47	\$	442,192.22	
516(1)	Drilled Shaft (equipment)	sub	10,222,642	3,492,471	13,715,113		0%	\$	-	\$	-	
516(2)	Unclassified Shaft Excavation	sub	1,629	204	1,833	CY	\$500	\$	588.45	\$	1,078,613.53	
516(3)	Rock Shaft Excavation	sub	3,723	1,542	5,265	CY	\$1,750	\$	2,059.58	\$	10,844,422.50	
516(4)	Casing (permanent steel)	sub	4,105,014	936,419	5,041,433	LB	\$0.65	\$	0.98	\$	4,940,604.73	REVISED PRICING
516(5)	Instrumentation and Data Collection	sub	128	48	176	EACH	\$1,750	\$	2,059.58	\$	362,485.20	
606(12)	Guardrail / Bridge Rail Connection	sub	4	4	8	EACH	\$1,500	\$	1,765.35	\$	14,122.80	
SP	Superstructure - Traveler Large	sup	1	1	2	EACH	\$500,000	\$	588,450.00	\$	1,176,900.00	
SP	Superstructure - Rent Traveler	sup	2	1	3	EACH	\$150,000	\$	176,535.00	\$	529,605.00	
SP	Pier Protection	sub	2	1.50	4	EACH	\$200,000	\$	235,380.00	\$	823,830.00	
	Lighting / Navigation Lighting	sup	1	1	2	LS	\$200,000	\$	235,380.00	\$	470,760.00	
	Size// as of Draiget Factor (Constructions)		0.0			Т	otal Bridge Cost=			\$	194,823,389.18	
	Size/Loc of Project Factor (Concr unit cost)=		0.9				Total SF Cost=			\$	04 004 004 44	
	Size/Loc of Project Factor (Rebar unit cost)=		0.95				Superstructure=			*	91,221,694.44	
			<b>F</b> +	10/	<b>T</b> - 4 - 1		Substructure=			\$	103,601,694.74	
	00.004.407		East	West	Total		Total SF Cost=		000 504		648.155496	
	26,031,137	Width	3,400	2,465	5,865 51.25		Area=		300,581		300,581	
		Area-SF	174,250	126,331	300,581		Contigency=				20%	
							Contigency=			\$	38,964,677.84	
							Rounding			\$	828.98	
						(does n	ot include costs fo	or co	fferdams, bubb	olers, a	and form travelers)	
							Total=		:	\$	233,788,896.00	
1							Total SF Cost=			\$	777.79	
1							Superstructure=			\$	364.18	
							Substructure=			\$	413.61	

AND BUBI	BLER SYS	TEM																	
					SHEETPILE	WALES	SPUD	WEIGHT	LA	BOR	EQU	P	MATERIALS		ABOR	-	EQUIP	MA	TERIALS
	#	L	W	н	SF			PZ-27		-					-				
PIER	3	56	56	60								_		-					
	4	76	68											-					
		4 00			44.400			583,200											
		4 60		60	14,400			583,200						-					
		2 80		110	17,600			712,800											
		2 72		110	15,840			641,520	_					_					
WALE		4 60		150		36,000								-					
		4 80		150		48,000													
		4 72		150		43,200								_					
SPUDS	1	2 80		128			122,880							-					
	1	2 120		128															
		_			47,840	127,200	122,880	1,937,520						-					
						,	,												
SPUDS WALE	UNIT	LF		MH/EA	24	384 763				100.00				\$	38,400		76,800		73,728 127,200
PILE	UNIT	TON SF		MH/UNIT MH/UNIT	64 47,840	9,568				800.00 100.00				\$ \$	610,560 956,800		305,280 956,800		775,008
MISC EXP	UNIT		\$ 1.00		47,040	3,500			Ψ	100.00	\$ 100	.00	\$ 0.40	Ψ	330,000	Ψ	330,000	\$	47,840
BUBBLE CURTAIN			\$ 5.00		47,840													\$	239,200
														\$	1,605,760	\$	1,338,880	\$	1,262,976
																		\$	4,207,616
							"DEEP WATE	R" PIER (~110')	_		14,	400		-				\$	1,266,506
								ATER" PIER (~			33,							\$	2,941,110
									- /		,								